

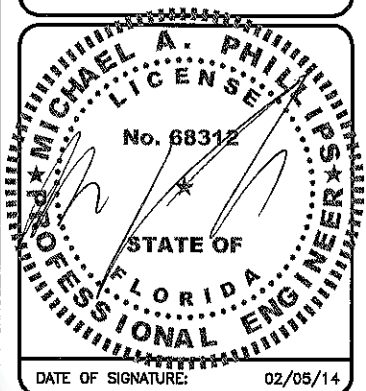
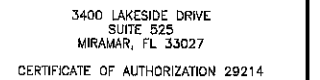


FLO1

3601 VINKEMULDER ROAD
COCONUT CREEK, FL 33073

3rd CARRIER OVERLAY

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FL01

3601 VINKEMULDER ROAD
COCONUT CREEK, FL 33073

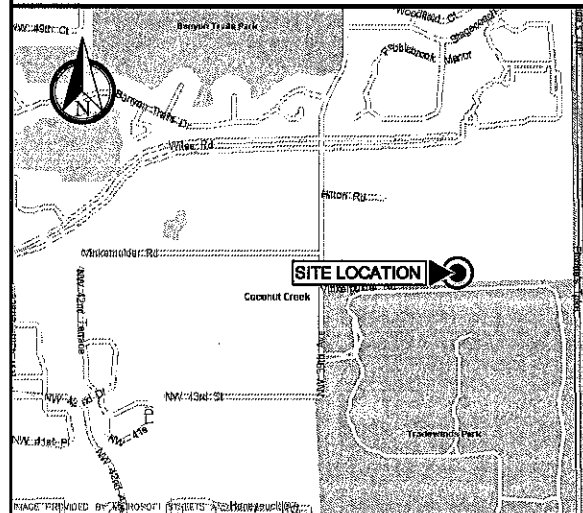
SHEET NAME

TITLE SHEET

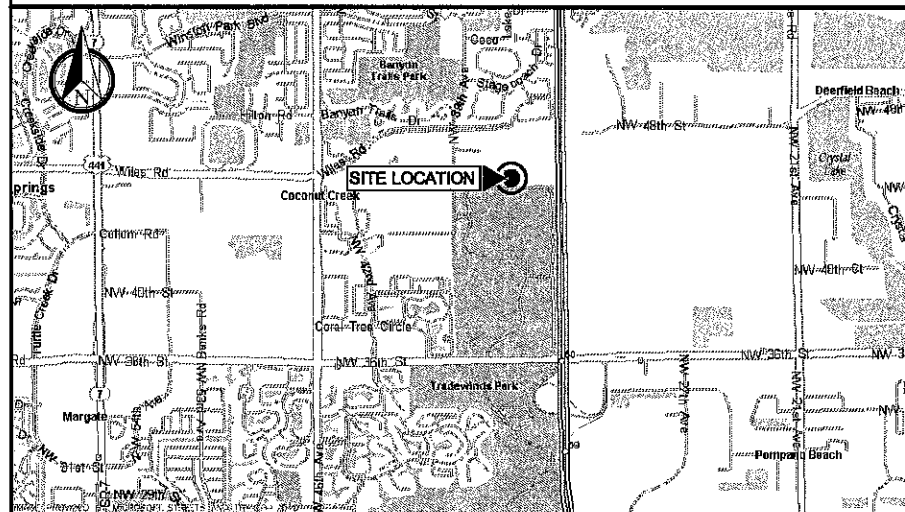
SHEET NUMBER

T1

LOCAL MAP



VICINITY MAP



DRIVING DIRECTIONS

FROM MASTEC'S BOCA RATON OFFICE HEAD SOUTH ON I-95 FOR 8.5 MILES TO EXIT 39 (SR-834/SAMPLE RD), HEAD WEST ON SAMPLE FOR 3.7 MILES TO NW 46th AVE (LYONS RD), TURN RIGHT AND HEAD NORTH ON LYONS FOR 0.8 MILES TO WILES RD, TURN RIGHT AND HEAD EAST ON WILES FOR 0.7 MILES TO NW 39th AVE, TURN RIGHT AND HEAD SOUTH ON 39th FOR 0.3 MILES TO VINKEMULDER RD, TURN LEFT AND HEAD EAST ON VINKEMULDER FOR 0.2 MILES TO SITE ON LEFT SIDE OF ROAD.

PROPERTY SUMMARY

FOLIO #:	4842-17-02-0010
LATITUDE:	26.285308° N
LONGITUDE:	80.172783° W
ZONING JURISDICTION:	CITY OF COCONUT CREEK
ZONING CLASSIFICATION:	AGRICULTURAL DISTRICT

CONTACTS

APPLICANT

MIKE KRISSEL
AT&T MOBILITY
5201 CONGRESS AVENUE
BOCA RATON, FL 33487
(561) 451-7496

PROPERTY OWNER

FLORIDA CELLULAR PHONE C/O AT&T WIRELESS
P.O. BOX 97061
REDMOND, WA 98073

RF DESIGN VERIFICATION

DESIGN BASED ON RFDS REV 0.2
DATED 11/21/13. CONTRACTOR SHALL
REQUEST CURRENT RFDS AND
WORKBOOK FROM MASTEC NETWORK
SOLUTIONS CONSTRUCTION MANAGER
PRIOR TO CONSTRUCTION

PROJECT INFORMATION

1. THIS IS AN UNMANNED FACILITY AND WILL BE USED FOR THE TRANSMISSION OF RADIO SIGNALS FOR THE PURPOSE OF PROVIDING PUBLIC CELLULAR SERVICE.
2. NO POTABLE WATER SUPPLY IS TO BE PROVIDED AT THIS LOCATION.
3. NO WASTEWATER WILL BE GENERATED AT THIS LOCATION.
4. NO SOLID WASTE WILL BE GENERATED AT THIS LOCATION.

DESIGN CRITERIA

DESIGN WIND SPEED: 170 MPH (ULTIMATE, 3-SECOND GUST)
132 MPH (NOMINAL, 3-SECOND GUST)
EXPOSURE: C
RISK CATEGORY: II
OPEN STRUCTURE

CODE COMPLIANCE

ALL WORK AND MATERIALS SHALL BE PERFORMED AND INSTALLED IN ACCORDANCE WITH THE CURRENT EDITIONS OF THE FOLLOWING CODES AS ADOPTED BY THE LOCAL GOVERNING AUTHORITIES. NOTHING IN THESE PLANS IS TO BE CONSTRUED TO PERMIT WORK NOT CONFORMING TO THESE CODES.

1. 2010 FLORIDA BUILDING CODE WITH 2012 SUPPLEMENT.
2. NATIONAL FIRE PROTECTION ASSOCIATION (NFPA) 70, NATIONAL ELECTRICAL CODE, 2008 EDITION.
3. TIA-222-G WITH ADDENDUM 1 APPLICABLE STANDARDS.
4. LIFE SAFETY CODE NFPA-101-2009.
5. 2010 FLORIDA FIRE PREVENTION CODE.
6. AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC) 360-05 AND 341-05.
7. UNDERWRITERS LABORATORIES (U.L.) APPROVED ELECTRICAL PRODUCTS.
8. LOCAL JURISDICTIONAL REQUIREMENTS.
9. CITY/COUNTY ORDINANCES.

NOTE:

THERE SHALL BE NO PIPES, CONDUITS OR CABLES RAN
THROUGH THE STAIRS OR ITS ENVELOPE.

LEGAL DESCRIPTION

COCONUT CREEK CELL SITE "A" 126-31 B & 17-48-42
PARCEL A & TOGETHER WITH E 75 OF S 100 OF: NW1/4 OF
NE1/4 SEC 17 & WITH S 20 OF: NW1/4 OF NE1/4 LESS IN
1058.20 & LESS W 1152.90 & LESS P/P/A 126-13 B

SCOPE OF WORK

1. REMOVAL OF (6) EXISTING AT&T ANTENNAS.
2. INSTALLATION OF (9) NEW AT&T ANTENNAS.
3. INSTALLATION OF (6) NEW REMOTE RADIO HEADS (RRHs).
4. INSTALLATION OF (2) NEW SURGE SUPPRESSORS.
5. INSTALLATION OF (3) NEW ANTENNA MOUNTS (WILL CAUSE THE SITE BE OFF-AIR FOR APPROXIMATELY 3 TO 7 DAYS).



ADMINISTRATIVE APPROVAL 02-24-14
APPROVED

1. FOR THE PURPOSES OF THESE CONSTRUCTION DRAWINGS, THE FOLLOWING DEFINITIONS SHALL APPLY:

OWNER - AT&T MOBILITY
ENGINEER - CALTROP CORPORATION
CONTRACTOR - GENERAL CONTRACTOR (CONSTRUCTION)

2. PRIOR TO SUBMITTING HIS BID, THE CONTRACTOR SHALL VISIT THE JOB SITE IN ORDER TO (1) VERIFY ALL EXISTING CONDITIONS, (2) CONFIRM WHETHER ALL DIMENSIONS ARE AS SHOWN ON THE PLANS AND (3) CONFIRM WHETHER THE WORK MAY BE ACCOMPLISHED AS SHOWN. ANY DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE CONSTRUCTION MANAGER.
3. A 20—FOOT HORIZONTAL CLEARANCE DISTANCE SHALL BE MAINTAINED FROM ALL EXISTING POWER LINES.
4. THE CONTRACTOR'S USE OF A CONSTRUCTION STAGING AREA SHALL BE COORDINATED WITH THE OWNER WELL IN ADVANCE OF THE CONSTRUCTION START DATE.
5. LABOR, MATERIAL, TOOLS, EQUIPMENT, TRANSPORTATION AND TEMPORARY POWER SERVICES NECESSARY FOR AN INCIDENTAL TO COMPLETION OF ALL WORK SHALL BE PROVIDED AS INDICATED ON THE DRAWINGS AND/OR AS SPECIFIED HEREIN. LABOR AND MATERIALS SHALL BE FURNISHED AS REQUIRED FOR COMPLETE SYSTEMS, INCLUDING ALL ELEMENTS OBVIOUSLY OR REASONABLY INCIDENTAL TO A COMPLETE INSTALLATION, WHETHER OR NOT SPECIFICALLY INDICATED ON THE PLANS.
6. FOR TASKS REQUIRED TO BE PERFORMED BUT NOT CLEARLY DEFINED OR IDENTIFIED BY THE CONTRACT DOCUMENTS, THE CONTRACTOR SHALL NOT START WORK ON SUCH TASKS WITHOUT HAVING RECEIVED WRITTEN AUTHORIZATION FROM THE CONSTRUCTION MANAGER TO PROCEED.
7. THE DRAWINGS ARE DIAGRAMMATIC AND INDICATE THE GENERAL ARRANGEMENT OF SYSTEMS AND EQUIPMENT UNLESS OTHERWISE INDICATED BY DIMENSIONS OR DETAILS. EXACT EQUIPMENT LOCATIONS MAY BE MODIFIED AS REQUIRED BY ACTUAL FIELD CONDITIONS. IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, CONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION FOR APPROVAL BY THE ENGINEER AND THE CONSTRUCTION MANAGER.
8. THE CONTRACTOR SHALL OBTAIN, PAY FOR AND DELIVER ALL REQUIRED PERMITS, CERTIFICATES OF INSPECTION, INCLUDING UTILITY CONNECTION FEES, ETC., REQUIRED BY THE AUTHORITIES HAVING JURISDICTION AND SHALL DELIVER SUCH DOCUMENTS TO THE OWNER PRIOR TO FINAL ACCEPTANCE OF THE WORK.
9. THE CONTRACTOR'S OPERATIONS SHALL BE CONFINED TO AREAS OF NEW CONSTRUCTION.
10. ALL NECESSARY PROVISIONS SHALL BE MADE TO PROTECT EXISTING IMPROVEMENTS, PAVING, CURBS, GALVANIZED SURFACES, ETC, AND THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY DAMAGE TO SAME RESULTING FROM THE CONSTRUCTION WORK. ALL DISTURBED AND DAMAGED AREAS SHALL BE RESTORED TO THEIR ORIGINAL CONDITION OR BETTER UPON COMPLETION OF ALL WORK TO THE SATISFACTION OF THE CONSTRUCTION MANAGER.
11. THE FOLLOWING CLEANUP TASKS SHALL BE PERFORMED AS FOLLOWS: (1) ON A DAILY BASIS, KEEP THE GENERAL AREA CLEAN AND HAZARD FREE, REMOVING ALL WASTE, DEBRIS AND TRASH FROM THE SITE AND DISPOSING OF SAME IN A LEGAL MANNER. (2) UPON COMPLETION, LEAVE THE PREMISES IN A CLEAN CONDITION AND FREE FROM PAINT SPOTS, DUST, OR SMUDGES OF ANY NATURE.
12. ALL EQUIPMENT AND MATERIALS SHALL BE INSTALLED IN ACCORDANCE WITH THE RESPECTIVE MANUFACTURER'S RECOMMENDATIONS EXCEPT WHERE IT IS SPECIFICALLY INDICATED OTHERWISE IN THE CONTRACT DOCUMENTS OR WHERE LOCAL CODES OR REGULATIONS TAKE PRECEDENCE.
13. ALL WORK PERFORMED AND MATERIALS INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS AND ORDINANCES. THE CONTRACTOR SHALL GIVE ALL NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY HAVING JURISDICTION OVER THE PERFORMANCE OF THE WORK. MECHANICAL AND ELECTRICAL SYSTEMS SHALL BE INSTALLED IN ACCORDANCE WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AS WELL AS LOCAL AND STATE CODES, ORDINANCES AND APPLICABLE REGULATIONS.
14. THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AT ALL TIMES, USING THE BEST SKILLS AND ATTENTION. HE SHALL BE SOLELY RESPONSIBLE FOR ALL OF THE CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES AND PROCEDURES AND FOR COORDINATING ALL PORTIONS OF THE WORK, INCLUDING CONTACT AND COORDINATION WITH THE CONSTRUCTION MANAGER AND WITH THE OWNER'S AUTHORIZED REPRESENTATIVE.
15. WITHIN TWENTY ONE (21) WORKING DAYS AFTER PROJECT COMPLETION, THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF AS—BUILT DRAWINGS, SWEEP TEST, CYLINDER TESTS, LIEN RELEASES, AND OTHER CLOSEOUT DOCUMENTATION AS REQUIRED BY THE OWNER. ALL SYSTEMS SHALL BE COMPLETELY ASSEMBLED, TESTED, ADJUSTED AND DEMONSTRATED TO BE READY FOR OPERATION PRIOR TO THE OWNER'S ACCEPTANCE.

GENERAL NOTES

1

1. THE APPROPRIATE UTILITY LOCATING SERVICES SHALL BE CONTACTED PRIOR TO THE START OF CONSTRUCTION IN ORDER TO VERIFY THE EXACT LOCATION OF ALL EXISTING UNDERGROUND UTILITIES.
2. THE INSTALLATION OF NEW UTILITIES SHALL BE COORDINATED WITH LOCAL AUTHORITIES.
3. ALL EXISTING ACTIVE SEWER, WATER, GAS, ELECTRIC AND OTHER UTILITIES, WHERE ENCOUNTERED IN THE WORK, SHALL BE PROTECTED AT ALL TIMES. WHERE REQUIRED FOR THE PROPER EXECUTION OF THE WORK, SUCH UTILITIES SHALL BE RELOCATED AS DIRECTED BY THE CONSTRUCTION MANAGER. EXTREME CAUTION SHALL BE USED WHEN EXCAVATING OR DRILLING PIERS AROUND OR NEAR UTILITIES.
4. RUBBISH, STUMPS, DEBRIS, STICKS, STONES AND OTHER REFUSE SHALL BE REMOVED FROM THE SITE AND DISPOSED OF LEGALLY.
5. ALL EXISTING INACTIVE SEWER, WATER, GAS, ELECTRIC AND OTHER UTILITIES THAT INTERFERE WITH THE EXECUTION OF THE WORK SHALL BE REMOVED AND/OR CAPPED, PLUGGED OR OTHERWISE DISCONTINUED AT POINTS THAT WILL NOT INTERFERE WITH THE EXECUTION OF THE WORK, SUBJECT TO THE APPROVAL OF THE LANDLORD AND/OR LOCAL UTILITIES.
6. DISTURBANCE TO THE EXISTING SITE DURING CONSTRUCTION SHALL BE MINIMIZED.
7. ANY AREAS OF THE CONSTRUCTION SITE DISTURBED BY THE WORK AND NOT COVERED BY THE TOWER, EQUIPMENT OR DRIVEWAY, SHALL BE GRADED TO A UNIFORM SLOPE. SUCH GRADING SHALL CAUSE SURFACE WATER TO FLOW AWAY FROM ANY EQUIPMENT SHELTER AND TOWER AREAS AND THE SOIL SHALL BE STABILIZED TO PREVENT EROSION. EROSION CONTROL MEASURES, IF REQUIRED DURING CONSTRUCTION, SHALL BE IN CONFORMANCE WITH THE LOCAL GUIDELINES FOR EROSION AND SEDIMENT CONTROL.
8. THE SUB-GRADE SHALL BE COMPACTED AND BROUGHT TO A UNIFORM GRADE PRIOR TO FINISHED SURFACE APPLICATION.
9. BACKFILL SHALL CONSIST OF CLEAN SAND FILL APPROVED FOR USE BY THE ENGINEER. NO UNAPPROVED MATERIAL WILL BE ALLOWED. CLEAN SAND FILL SHALL BE FREE OF ALL ROOTS, BOULDERS, OR OTHER DELETERIOUS MATERIAL.
10. THE CONTRACTOR SHALL RESTORE ALL DISTURBED AREAS TO EQUAL TO OR BETTER CONDITION THAN ORIGINAL.
11. SITE SIGNAGE SHALL BE PROVIDED IN ACCORDANCE WITH THE TECHNICAL SPECIFICATIONS FOR SUCH SIGNAGE AS MAY BE CONTAINED IN THESE DRAWINGS.

SITE WORK NOTES

2

1. MATERIAL:
 - A. ALL STRUCTURAL STEEL WORK SHALL CONFORM TO THE LATEST EDITION OF THE AISC "STEEL CONSTRUCTION MANUAL".
 - B. ALL STRUCTURAL STEEL WF BEAMS SHALL BE ASTM A992 AND "HOT DIPPED" GALVANIZED IN ACCORDANCE WITH ASTM A123 AND ASTM A153 STANDARDS.
 - C. ALL STRUCTURAL PLATES, ANGLES, AND CHANNELS SHALL BE ASTM A36 AND "HOT DIPPED" GALVANIZED IN ACCORDANCE WITH ASTM A123 AND ASTM A153 STANDARDS.
 - D. ALL TS MEMBERS SHALL BE ASTM A500 GRADE B ($F_y=46\text{ksi}$), AND "HOT DIPPED" GALVANIZED IN ACCORDANCE WITH ASTM A123 AND ASTM A153 STANDARDS.
 - E. ALL STRUCTURAL PIPE MEMBERS SHALL BE ASTM A500 GRADE B ($F_y=42\text{ksi}$), AND "HOT DIPPED" GALVANIZED IN ACCORDANCE WITH ASTM A123 AND ASTM A153 STANDARDS.
 - F. ALL NON-STRUCTURAL PIPE MEMBERS SHALL BE ASTM A53 GRADE B, AND "HOT DIPPED" GALVANIZED IN ACCORDANCE WITH ASTM A123 AND ASTM A153 STANDARDS.
2. DESIGN, FABRICATION, AND CONSTRUCTION OF ALL CONNECTIONS SHALL CONFORM TO AISC STEEL CONSTRUCTION MANUAL.
3. WELDING:
 - A. ALL WELDS, WELDERS, AND WELD INSPECTIONS SHALL CONFORM TO THE REQUIREMENTS OF AWS D 1.1, LATEST REVISION.
 - B. ALL WELDS SHALL BE MADE WITH E70XX LOW HYDROGEN ELECTRODES.
 - C. ALL STEEL SHALL BE SPRAY GALVANIZED AFTER WELDING.
4. ALL BOLTS SHALL BE GALVANIZED $\frac{3}{4}$ " DIAMETER, A325-N, UNLESS NOTED OTHERWISE AND TIGHTENED TO A "SNUG TIGHT" CONDITION AS DEFINED BY AISC. SECURE NUT WITH LOCKING WASHER.
5. ANCHOR BOLTS SHALL CONFORM TO ASTM A307, UNLESS NOTED OTHERWISE.
6. THE CONTRACTOR/STEEL FABRICATOR SHALL LOCATE ANY REINFORCEMENT IN THE STRUCTURAL MEMBERS IN SUCH A MANNER SO THAT THERE WILL NOT BE CONFLICT WITH THE REINFORCEMENT WHEN INSTALLING ANCHORS. THE ANCHORS SHALL BE INSTALLED PER THE MANUFACTURER'S INSTRUCTION.
7. THE CONTRACTOR/STEEL FABRICATOR SHALL CONFORM TO THE MINIMUM EDGE DISTANCE REQUIREMENTS IN ACCORDANCE WITH THE AISC MANUAL OF STEEL CONSTRUCTION.
8. ALL STRUCTURAL STEEL SHALL BE FABRICATED TO FIT AT BOLTED CONNECTIONS WITHIN $\frac{1}{16}$ INCH TOLERANCE. STRUCTURAL STEEL SHALL NOT BE FLAME CUT UNDER ANY CIRCUMSTANCES WITHOUT APPROVAL OF THE ENGINEER.
9. THE CONTRACTOR/STEEL FABRICATOR SHALL CAP OR SEAL ALL PIPES AS REQUIRED TO PREVENT RAINWATER INTRUSION.
10. THE CONTRACTOR/STEEL FABRICATOR SHALL SUBMIT SHOP DRAWINGS FOR REVIEW PRIOR TO ANY STEEL FABRICATION. AT THE CONTRACTOR'S OPTION, FIELD SPLICES MAY BE USED FOR ERECTION PURPOSES. IF FIELD SPLICES ARE USED, THE SHOP DRAWINGS SHALL INCLUDE ALL DETAILS FOR THE PROPOSED FIELD SPLICES.
11. AT THE CONTRACTOR'S OPTION, SHOP WELDS MAY BE USED INSTEAD OF FIELD WELDS.
12. SUBMIT ORIGINAL SHOP DRAWINGS, INCLUDING COMPLETE DETAILS, SCHEDULES OF FABRICATION AND ASSEMBLY, PROCEDURES, AND DIAGRAMS. INCLUDE DETAILS OF CUTS, CONNECTIONS, CAMBER, HOLE, AND OTHER PERTINENT DATA. INDICATE WELDS BY STANDARD AWS A2.1 AND A2.4 SYMBOLS, AND SHOW SIZE, LENGTH, AND TYPE OF WELD. PROVIDE SETTING DRAWINGS, TEMPLATES, AND DIRECTIONS FOR INSTALLATION OF ANCHOR BOLTS AND OTHER ANCHORAGES TO BE INSTALLED AS WORK OF OTHERS' SECTIONS.

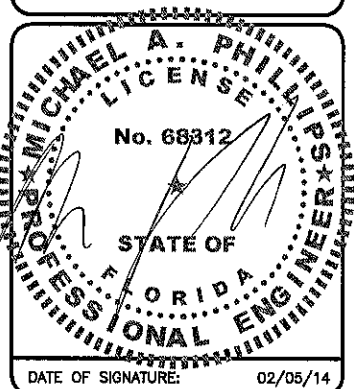
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3400 LAKESIDE DRIVE
SUITE 525
MIRAMAR, FL 33027

CERTIFICATE OF AUTHORIZATION 29214



FL01

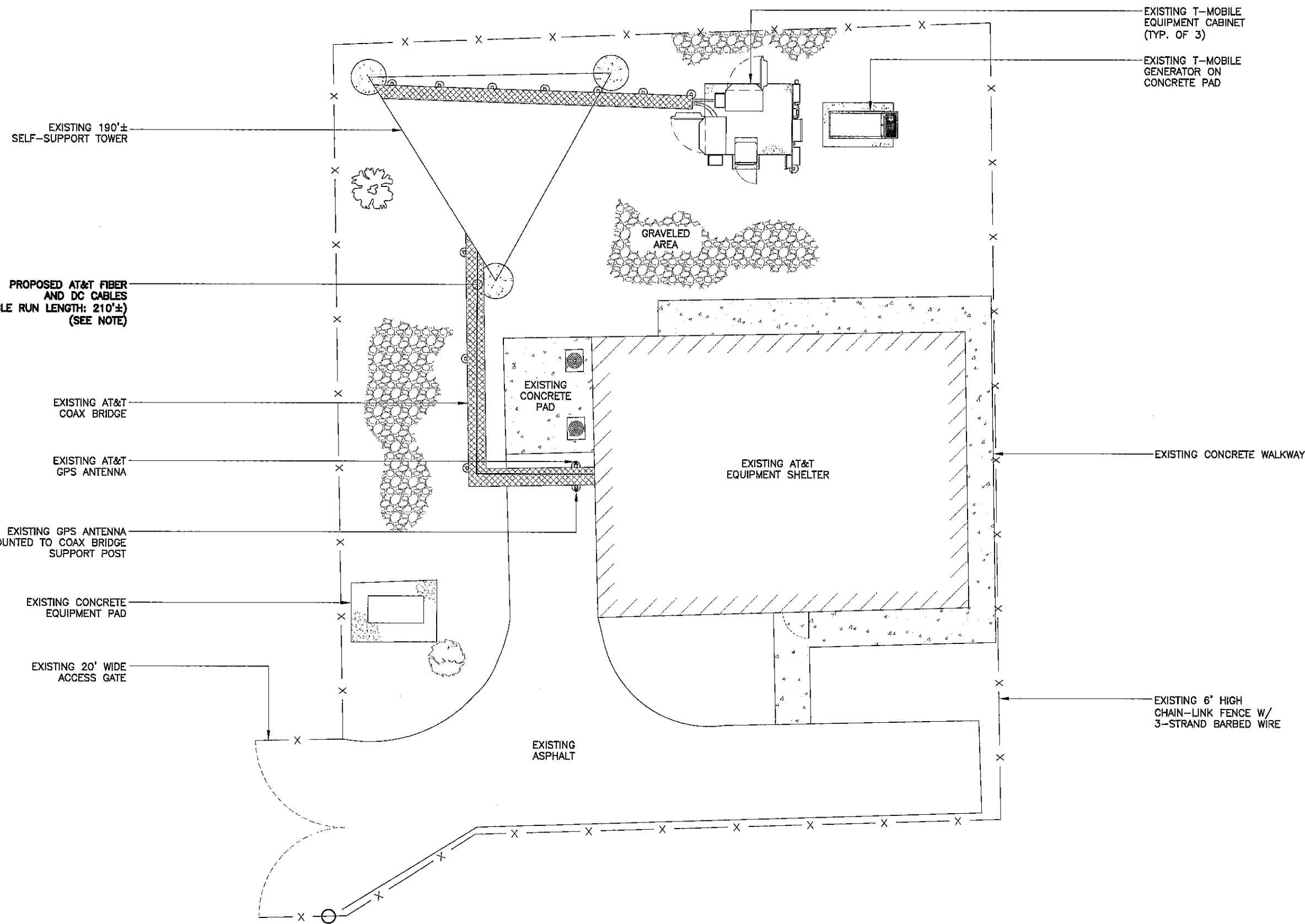
3601 VINKEMULDER ROAD
COCONUT CREEK, FL 33073

SHEET NAME

NOTES

SHEET NUMBER

C1

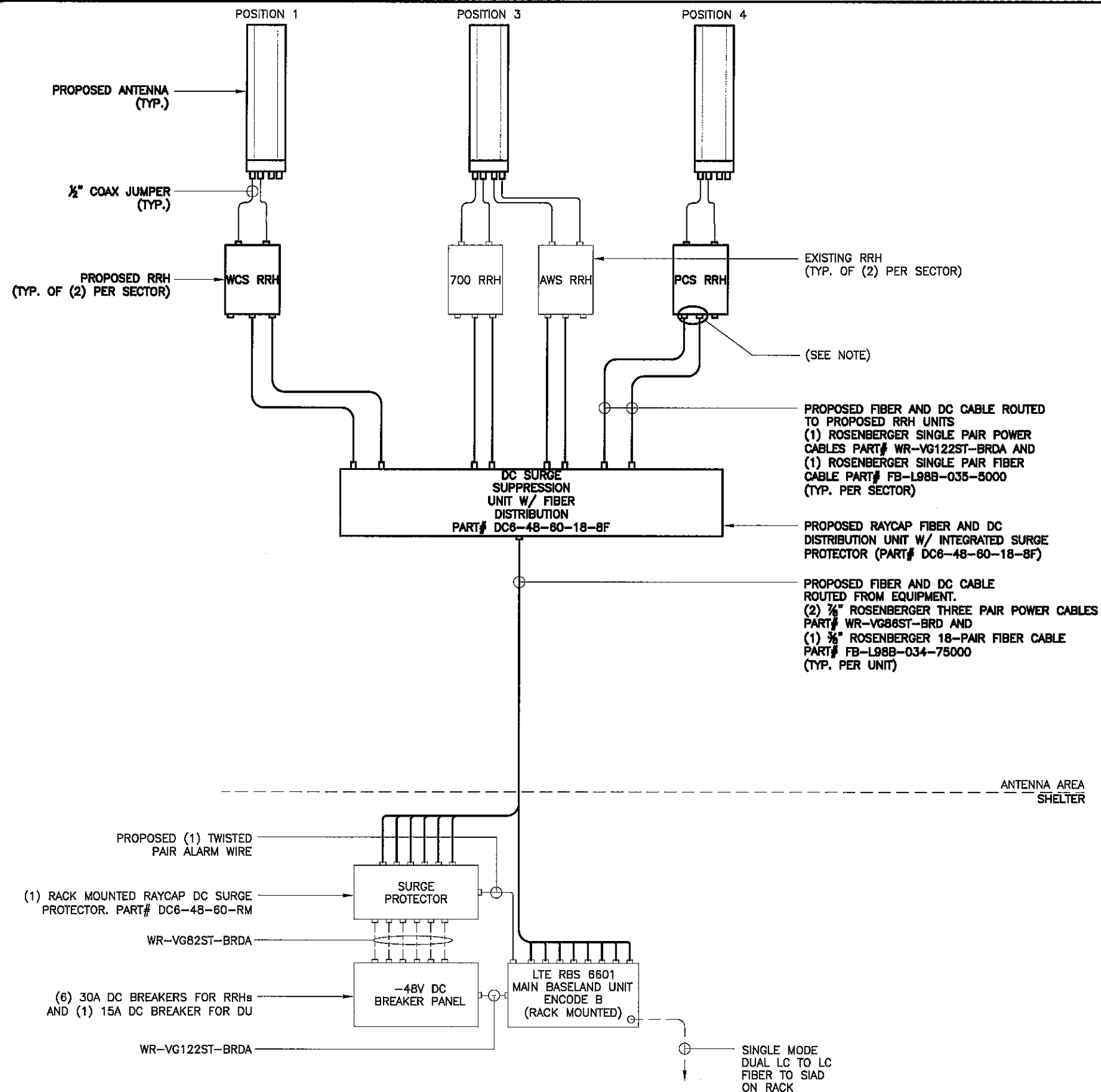


CONTRACTOR SHALL REMOVE EXISTING UNUSED CABLES
AS NEEDED TO CREATE SPACE FOR PROPOSED CABLES.

0 6'

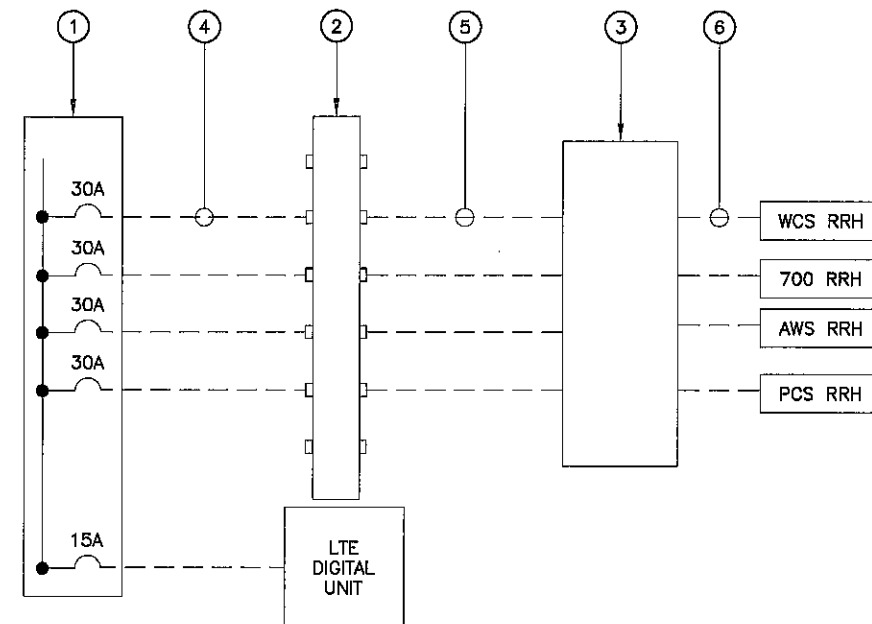
GRAPHIC SCALE

<p>FLO1</p> <p>3601 VINKEMULDER ROAD COCONUT CREEK, FL 33073</p>
<p>SHEET NAME</p> <p>COMPOUND PLAN</p>
<p>SHEET NUMBER</p> <p>C2</p>



- NOTES:

1. CONTRACTOR SHALL USE ERICSSON PROVIDED DC POWER CABLE CONNECTOR.
2. CONTRACTOR SHALL REMOVE EXISTING UNUSED CABLES AS NEEDED TO CREATE SPACE FOR PROPOSED CABLES.

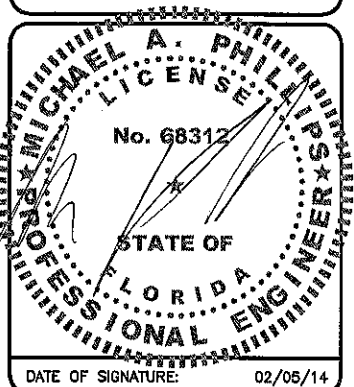


- KEYNOTE LEGEND:

1. -48V DC POWER PLANT.
2. (1) RACK MOUNTED RAYCAP DC SURGE PROTECTOR (DC6-48-60-RM).
3. RAYCAP FIBER AND DC DISTRIBUTION UNIT (DC6-48-60-18)
4. #8 AWG CONDUCTORS.
5. PROVIDE (2) 6-CONDUCTOR #8 AWG BUNDLES FOR DC POWER FROM RACK MOUNTED RAYCAP SURGE PROTECTION UNIT TO THE RAYCAP FIBER AND DISTRIBUTION UNIT ON TOWER
6. PROPOSED FIBER AND DC CABLE ROUTED TO PROPOSED RRH UNITS

[illegible]

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FL01

3601 VINKEMULDER ROAD
COCONUT CREEK, FL 33073

SHEET NAME

DC ELECTRICAL DETAILS

SHEET NUMBER

E1



MasTec Network Solutions
6100 Broken Sound Pkwy Suite 6
Boca Raton, FL 33487
(678) 896-9330



Kevin Clements
520 S. Main St., Suite 2531
Akron, Ohio 44311
(330) 572-2100
kclements@gpdgroup.com

GPD# 2013723.04.6990.02 Rev 1
February 3, 2014

REVISED RIGOROUS STRUCTURAL ANALYSIS REPORT

AT&T DESIGNATION: **Site USID:** **6990**
 Site FA: **10070109**
 Site Name: **FL01**
 AT&T Project: **MOD_LTE_3C_11-08-2013**

ANALYSIS CRITERIA: **Codes:** **TIA-222-G, 2009 IBC & 2010 FBC**
 132-mph Nominal 3-Second Gust with 0" ice
 170-mph Ultimate 3-Second Gust with 0" ice

SITE DATA: **3601 Vinkemulder Rd., Coconut Creek, FL 33073, Broward County**
 Latitude 26° 17' 5.978" N, Longitude 80° 10' 21.979" W
 Market: South Florida
 192.3' Rohn Self Support Tower

Ms. Bridget Rohack,

GPD is pleased to submit this Rigorous Structural Analysis Report to determine the structural integrity of the aforementioned tower. The purpose of the analysis is to determine the suitability of the tower with the existing and proposed loading configuration detailed in the analysis report.

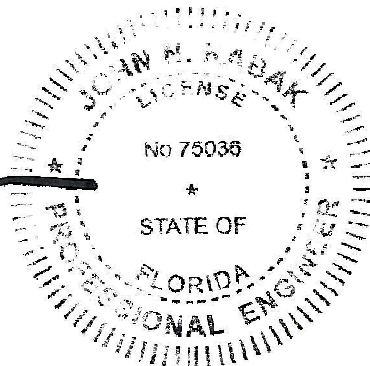
Analysis Results

Tower Stress Level with Proposed Equipment:	103.2%	Pass
Foundation Ratio with Proposed Equipment:	99.3%	Pass

We at GPD appreciate the opportunity of providing our continuing professional services to you and MasTec Network Solutions. If you have any questions or need further assistance on this or any other projects please do not hesitate to call.

Respectfully submitted,

John N. Kabak, S.E.
Florida #: 75036



SUMMARY & RESULTS

The purpose of this analysis was to verify whether the existing structure is capable of carrying the proposed loading configuration as specified by AT&T to MasTec Network Solutions. This report was commissioned by Ms. Bridget Rohack of MasTec Network Solutions.

The analysis has been performed in accordance with the 2010 Florida Building Code based upon a strength design wind speed of 170 mph and the ASCE 7-10. Wind loading was taken from the 2010 FBC in accordance with Section 1620: High Velocity Hurricane Zones, with Exposure Category C, Risk Category II and a nominal design wind speed of 132 mph 3-second gust.

Modifications by FDH project #: 11-07019E S3, dated 1/13/12, have not been installed and were not considered in this analysis.

Modifications designed by GPD Project #: 2012771.41, dated 6/27/12, have been considered in this analysis.

The proposed DC, Fiber and RET lines to 100' shall be installed with the existing DC, Fiber and RET lines to form a (4) on (4) configuration for the analysis results to be valid. See Appendix C for the coax layout.

TOWER SUMMARY AND RESULTS

Member	Capacity	Results
Legs	91.9%	Pass
Diagonals	103.2%	Pass
Horizontals	102.6%	Pass
Member Bolts	61.1%	Pass
Anchor Rods	90.6%	Pass
Foundation	99.3%	Pass

Note: Ratings at or below 105% are within standard engineering tolerances and therefore are considered satisfactory.

ANALYSIS METHOD

tnxTower (Version 6.1.3.1), a commercially available software program, was used to create a three-dimensional model of the tower and calculate primary member stresses for various dead, live and wind load cases. Selected output from the analysis is included in Appendix B. The following table details the information provided to complete this structural analysis. This analysis is solely based on this information and is being provided without the benefit of a recent site visit.

DOCUMENTS PROVIDED

Document	Remarks	Source
Equipment Modification Form	AT&T Internal Loading Document, uploaded 11/12/13	Siterra
Tower Design	Not Provided	N/A
Foundation Design	Not Provided	N/A
Geotechnical Report	Ground Down Engineering Job #: 11-488, dated 8/26/11	Siterra
Tower Mapping	FDH Job #: 11-07013T T1, dated 8/23/11	Siterra
Foundation Mapping	FDH Job #: 1107019EN1, dated 7/15/11	Siterra
Modification Design	FDH Job #: 11-07019E S3, dated 1/13/12	Siterra
Modification Design	GPD Job #: 2012771.41, dated 6/27/12	Siterra
Previous Structural Analysis	GPD Job #: 2013723.6990.01, dated 3/19/13	Siterra

ASSUMPTIONS

This rigorous structural analysis is based on the theoretical capacity of the members and is not a condition assessment of the tower. This analysis is from information supplied, and therefore, its results are based on and are as accurate as that supplied data. GPD has made no independent determination, nor is it required to, of its accuracy. The following assumptions were made for this structural analysis.

1. The tower member sizes and shapes are considered accurate as supplied. The material grade is as per data supplied and/or as assumed and as stated in the materials section.
2. The antenna configuration is as supplied and/or as modeled in the analysis. It is assumed to be complete and accurate. All antennas, mounts, coax and waveguides are assumed to be properly installed and supported as per manufacturer requirements.
3. Some assumptions are made regarding antennas and mount sizes and their projected areas based on best interpretation of data supplied and of best knowledge of antenna type and industry practice.
4. All mounts, if applicable, are considered adequate to support the loading. No actual analysis of the mount(s) is performed. This analysis is limited to analyzing the tower only.
5. The soil parameters are as per data supplied or as assumed and stated in the calculations.
6. Foundations are properly designed and constructed to resist the original design loads indicated in the documents provided.
7. The tower and structures have been properly maintained in accordance with TIA Standards and/or with manufacturer's specifications.
8. All welds and connections are assumed to develop at least the member capacity unless determined otherwise and explicitly stated in this report.
9. All prior structural modifications are assumed to be as per data supplied/available and to have been properly installed.
10. Loading interpreted from photos is accurate to $\pm 5'$ AGL, antenna size accurate to ± 3.3 sf, and coax equal to the number of existing antennas without reserve.
11. All existing loading was obtained from the previous analysis by GPD Job #: 2013723.6990.01, dated 3/19/13, site photos, the provided EMF and is assumed to be accurate.
12. Modifications by FDH project #: 11-07019E S3, dated 1/13/12 have not been installed and were not considered in this analysis.
13. Modifications designed by GPD Project #: 2012771.41, dated 6/27/12, have been considered in this analysis.
14. Leg A is assumed to be at 50° per the tower mapping by FDH (Job #: 11-07013T T1, dated 1/13/12).
15. The loading considered in this analysis was confirmed through email correspondence with Ms. Bridget Rohack of MasTec Network Solutions, dated 11/23/13.

If any of these assumptions are not valid or have been made in error, this analysis may be affected, and GPD Group should be allowed to review any new information to determine its effect on the structural integrity of the tower.

DISCLAIMER OF WARRANTIES

GPD GROUP has not performed a site visit to the tower to verify the member sizes or antenna/coax loading. If the existing conditions are not as represented on the tower elevation contained in this report, we should be contacted immediately to evaluate the significance of the discrepancy. This is not a condition assessment of the tower or foundation. This report does not replace a full tower inspection. The tower and foundations are assumed to have been properly fabricated, erected, maintained, in good condition, twist free, and plumb.

The engineering services rendered by GPD GROUP in connection with this Rigorous Structural Analysis are limited to a computer analysis of the tower structure and theoretical capacity of its main structural members. All tower components have been assumed to only resist dead loads when no other loads are applied. No allowance was made for any damaged, bent, missing, loose, or rusted members (above and below ground). No allowance was made for loose bolts or cracked welds.

GPD GROUP does not analyze the fabrication of the structure (including welding). It is not possible to have all the very detailed information needed to perform a thorough analysis of every structural sub-component and connection of an existing tower. GPD GROUP provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc. The purpose of this report is to assess the feasibility of adding appurtenances usually accompanied by transmission lines to the structure.

It is the owner's responsibility to determine the amount of ice accumulation in excess of the specified code recommended amount, if any, that should be considered in the structural analysis.

The attached sketches are a schematic representation of the analyzed tower. If any material is fabricated from these sketches, the contractor shall be responsible for field verifying the existing conditions, proper fit, and clearance in the field. Any mentions of structural modifications are reasonable estimates and should not be used as a precise construction document. Precise modification drawings are obtainable from GPD GROUP, but are beyond the scope of this report.

Miscellaneous items such as antenna mounts, etc., have not been designed or detailed as a part of our work. We recommend that material of adequate size and strength be purchased from a reputable tower manufacturer.

GPD GROUP makes no warranties, expressed and/or implied, in connection with this report and disclaims any liability arising from material, fabrication, and erection of this tower. GPD GROUP will not be responsible whatsoever for, or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of GPD GROUP pursuant to this report will be limited to the total fee received for preparation of this report.

APPENDIX A

Tower Analysis Summary Form

[illegible]

APPENDIX B

tnxTower Output File

tnxTower GPD Group 520 South Main St. Suite 2531 Akron, OH 44311 Phone: (330) 572-2100 FAX: (330) 572-2101	Job	6990 FL01	Page	1 of 7
	Project	2013723.04.6990.02	Date	07:25:09 11/25/13
	Client	MasTec Network Solutions	Designed by	mhoudeshell

Tower Input Data

The main tower is a 3x free standing tower with an overall height of 192.33 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 7.50 ft at the top and 28.00 ft at the base.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

Tower is located in Broward County, Florida.

Basic wind speed of 132 mph.

Structure Class II.

Exposure Category C.

Topographic Category 1.

Crest Height 0.00 ft.

Deflections calculated using a wind speed of 60 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in tower member design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
Lighting Cables	B	No	Ar (CaAa)	192.30 - 8.00	0.0000	0.21	1	1	0.7500	0.7500		0.33
LDF7-50A (1-5/8 FOAM)	B	No	Ar (CaAa)	190.00 - 8.00	0.0000	0.43	2	2	1.0000	1.9800		0.82
LDF5-50A (7/8 FOAM)	B	No	Ar (CaAa)	190.00 - 8.00	2.5000	0.43	2	2	1.0000	1.0900		0.33
Feedline Ladder (Af)	B	No	Af (CaAa)	190.00 - 8.00	0.0000	0.45	1	1	3.0000	3.0000		8.40
Feedline Ladder (Af)	B	No	Af (CaAa)	190.00 - 8.00	0.0000	0.25	1	1	3.0000	3.0000		8.40
Feedline Ladder (Af)	C	No	Af (CaAa)	190.00 - 8.00	0.0000	0.4	1	1	3.0000	3.0000		8.40
5/8" Step Bolts	A	No	Ar (CaAa)	190.00 - 8.00	0.0000	0.5	1	1	0.4167	0.4167		1.00
5/8" Step Bolts	B	No	Ar (CaAa)	190.00 - 8.00	0.0000	0.5	1	1	0.4167	0.4167		1.00
5/8" Step Bolts	C	No	Ar (CaAa)	190.00 - 8.00	0.0000	0.5	1	1	0.4167	0.4167		1.00
LDF7-50A (1-5/8 FOAM)	C	No	Ar (CaAa)	165.00 - 8.00	-0.7500	0.4	12	6	1.0000	1.9800		0.82
Hybrid 1-5/8	C	No	Ar (CaAa)	165.00 - 8.00	-0.7500	0.37	1	1	1.0000	1.5840		1.61
LDF5-50A (7/8 FOAM)	B	No	Ar (CaAa)	133.00 - 8.00	0.0000	0.2	1	1	1.0000	1.0900		0.33
LDF5-50A (7/8 FOAM)	B	No	Ar (CaAa)	100.00 - 8.00	0.0000	0.45	12	6	1.0000	1.0900		0.33
7/8" DC Power Cable	B	No	Ar (CaAa)	100.00 - 8.00	0.0000	0.22	6	2	0.8750	0.8750		0.60
3/8" Fiber Cable	B	No	Ar (CaAa)	100.00 - 8.00	0.0000	0.24	3	1	0.3750	0.3750		0.10
RET Cable	B	No	Ar (CaAa)	100.00 - 8.00	0.0000	0.25	3	1	0.4400	0.4400		0.08

<i>tnxTower</i> GPD Group 520 South Main St. Suite 2531 Akron, OH 44311 Phone: (330) 572-2100 FAX: (330) 572-2101	Job	6990 FL01	Page	2 of 7
	Project	2013723.04.6990.02	Date	07:25:09 11/25/13
	Client	MasTec Network Solutions	Designed by	mhoudeshell

Discrete Tower Loads

<i>Description</i>	<i>Face or Leg</i>	<i>Offset Type</i>	<i>Offsets: Horz Lateral Vert ft ft ft</i>	<i>Azimuth Adjustment °</i>	<i>Placement ft</i>		<i>C_{AA} Front ft²</i>	<i>C_{AA} Side ft²</i>	<i>Weight lb</i>
Flash Beacon Lighting	A	From Leg	0.00 0.00 0.00	0.0000	192.30	No Ice	2.70	2.70	50.00
8' Frame	B	From Leg	0.50 0.00 0.00	0.0000	189.00	No Ice	8.83	7.05	268.16
8' Frame	C	From Leg	0.50 0.00 0.00	0.0000	189.00	No Ice	8.83	7.05	268.16
16 Element 20' x 2" Dipole	B	From Leg	1.00 0.00 12.00	0.0000	189.00	No Ice	4.00	4.00	40.00
3 Element 18" x 12" Yagi	C	From Leg	1.00 0.00 6.50	0.0000	189.00	No Ice	0.07	0.07	5.00
3" x 8' Omni	C	From Leg	1.00 0.00 6.00	0.0000	189.00	No Ice	2.40	2.40	25.00
2" x 8' Omni	B	From Leg	1.00 0.00 6.00	0.0000	189.00	No Ice	1.60	1.60	20.00
11.5' T-Frame	A	From Leg	0.98 0.17 0.00	10.0000	165.00	No Ice	16.40	10.28	317.50
11.5' T-Frame	B	From Leg	0.98 0.17 0.00	10.0000	165.00	No Ice	16.40	10.28	317.50
11.5' T-Frame	C	From Leg	0.98 0.17 0.00	10.0000	165.00	No Ice	16.40	10.28	317.50
(3) APX17DWV-17DWV-S-E-A CU w/ Mount Pipe	A	From Leg	1.97 0.35 0.00	10.0000	165.00	No Ice	9.23	4.52	67.60
(3) APX17DWV-17DWV-S-E-A CU w/ Mount Pipe	B	From Leg	1.97 0.35 0.00	10.0000	165.00	No Ice	9.23	4.52	67.60
(3) APX17DWV-17DWV-S-E-A CU w/ Mount Pipe	C	From Leg	1.97 0.35 0.00	10.0000	165.00	No Ice	9.23	4.52	67.60
FRIG	A	From Leg	1.97 0.35 0.00	10.0000	165.00	No Ice	2.79	1.10	57.32
FRIG	B	From Leg	1.97 0.35 0.00	10.0000	165.00	No Ice	2.79	1.10	57.32
FRIG	C	From Leg	1.97 0.35 0.00	10.0000	165.00	No Ice	2.79	1.10	57.32
FXFB	A	From Leg	1.97 0.35 0.00	10.0000	165.00	No Ice	0.99	1.12	55.12
FXFB	B	From Leg	1.97 0.35 0.00	10.0000	165.00	No Ice	0.99	1.12	55.12

<i>tnxTower</i> <i>GPD Group</i> 520 South Main St. Suite 2531 Akrón, OH 44311 Phone: (330) 572-2100 FAX: (330) 572-2101	Job	6990 FL01	Page	3 of 7
	Project	2013723.04.6990.02	Date	07:25:09 11/25/13
	Client	MasTec Network Solutions	Designed by	mhoudeshell

<i>Description</i>	<i>Face or Leg</i>	<i>Offset Type</i>	<i>Offsets: Horz Lateral Vert ft ft ft</i>	<i>Azimuth Adjustment °</i>	<i>Placement ft</i>		<i>C_{AA} Front ft²</i>	<i>C_{AA} Side ft²</i>	<i>Weight lb</i>
FXFB	C	From Leg	1.97 0.35 0.00	10.0000	165.00	No Ice	0.99	1.12	55.12
FRIA	A	From Leg	1.97 0.35 0.00	10.0000	165.00	No Ice	4.13	0.98	55.00
FRIA	B	From Leg	1.97 0.35 0.00	10.0000	165.00	No Ice	4.13	0.98	55.00
FRIA	C	From Leg	1.97 0.35 0.00	10.0000	165.00	No Ice	4.13	0.98	55.00
RCMDC-4010-PF-48	A	From Leg	1.97 0.35 0.00	10.0000	165.00	No Ice	3.22	1.16	20.00
2' Standoff	A	From Leg	1.00 0.00 0.00	0.0000	133.00	No Ice	2.97	2.99	55.00
2" x 8' Omni	A	From Leg	2.00 0.00 4.00	0.0000	133.00	No Ice	1.60	1.60	20.00
1' Square Dish	A	From Leg	2.00 0.00 0.00	0.0000	133.00	No Ice	1.40	0.08	3.00
15' T-Boom	A	From Leg	1.15 1.64 0.00	55.0000	100.00	No Ice	23.51	10.62	641.88
15' T-Boom	B	From Leg	1.15 1.64 0.00	55.0000	100.00	No Ice	23.51	10.62	641.88
15' T-Boom	C	From Leg	1.15 1.64 0.00	55.0000	100.00	No Ice	23.51	10.62	641.88
(3) 800-10865 w/ Mount Pipe	A	From Leg	2.29 3.28 0.00	55.0000	100.00	No Ice	11.70	7.94	106.32
(3) 800-10865 w/ Mount Pipe	B	From Leg	2.29 3.28 0.00	55.0000	100.00	No Ice	11.70	7.94	106.32
(3) 800-10865 w/ Mount Pipe	C	From Leg	2.29 3.28 0.00	55.0000	100.00	No Ice	11.70	7.94	106.32
(3) RRUS-32	A	From Leg	2.29 3.28 0.00	55.0000	100.00	No Ice	3.87	2.76	77.00
(3) RRUS-32	B	From Leg	2.29 3.28 0.00	55.0000	100.00	No Ice	3.87	2.76	77.00
(3) RRUS-32	C	From Leg	2.29 3.28 0.00	55.0000	100.00	No Ice	3.87	2.76	77.00
RRUS 11	A	From Leg	2.29 3.28 0.00	55.0000	100.00	No Ice	3.25	1.37	50.70
RRUS 11	B	From Leg	2.29 3.28 0.00	55.0000	100.00	No Ice	3.25	1.37	50.70

tnxTower GPD Group 520 South Main St. Suite 2531 Akron, OH 44311 Phone: (330) 572-2100 FAX: (330) 572-2101	Job	6990 FL01	Page	4 of 7
	Project	2013723.04.6990.02	Date	07:25:09 11/25/13
	Client	MasTec Network Solutions	Designed by	mhoudeshell

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft		C _{AA} Front ft ²	C _{AA} Side ft ²	Weight lb
RRUS 11	C	From Leg	2.29 3.28 0.00	55.0000	100.00	No Ice	3.25	1.37	50.70
DC6-48-60-18-8F Surge Suppression Unit	A	From Leg	2.29 3.28 0.00	55.0000	100.00	No Ice	1.47	1.47	18.90
DC6-48-60-18-8F Surge Suppression Unit	B	From Leg	2.29 3.28 0.00	55.0000	100.00	No Ice	1.47	1.47	18.90
DC6-48-60-18-8F Surge Suppression Unit	C	From Leg	2.29 3.28 0.00	55.0000	100.00	No Ice	1.47	1.47	18.90

Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
192.30	Flash Beacon Lighting	32	2.367	0.1114	0.0167	583677
189.00	8' Frame	32	2.290	0.1113	0.0165	583677
165.00	11.5' T-Frame	32	1.732	0.1049	0.0110	106459
133.00	2' Standoff	32	1.098	0.0777	0.0060	62703
100.00	15' T-Boom	32	0.631	0.0569	0.0041	114466

Bolt Design Data

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt lb	Allowable Load lb	Ratio Load Allowable	Allowable Ratio	Criteria
T1	192.333	Leg	A325N	0.7500	4	325.56	29820.60	0.011	1	Bolt Tension
		Diagonal	A325N	0.5000	3	779.64	7952.16	0.098	1	Bolt Shear
		Horizontal	A325N	0.6250	3	497.36	12425.20	0.040	1	Bolt Shear
T2	182.167	Leg	A325N	0.7500	4	3161.69	29820.60	0.106	1	Bolt Tension
		Diagonal	A325N	0.5000	3	2452.47	7952.16	0.308	1	Bolt Shear
		Horizontal	A325N	0.6250	3	1218.29	12425.20	0.098	1	Bolt Shear
T3	162	Leg	A325N	0.8750	4	11357.00	40589.10	0.280	1	Bolt Tension
		Diagonal	A325N	0.5000	3	3098.73	7952.16	0.390	1	Bolt Shear
		Horizontal	A325N	0.6250	3	1754.13	12425.20	0.141	1	Bolt Shear
T4	141.833	Leg	A325N	1.0000	4	19375.70	53014.40	0.365	1	Bolt Tension
		Diagonal	A325N	0.5000	3	2968.50	7952.16	0.373	1	Bolt Shear
		Horizontal	A325N	0.6250	3	2009.62	12425.20	0.162	1	Bolt Shear
T5	121.625	Leg	A325N	1.0000	6	17265.00	53014.40	0.326	1	Bolt Tension
		Diagonal	A325N	0.5000	3	3844.74	7952.16	0.483	1	Bolt Shear
		Horizontal	A325N	0.6250	3	2288.41	12425.20	0.184	1	Bolt Shear
T6	101.417	Leg	A325N	1.0000	6	23062.90	53014.40	0.435	1	Bolt Tension

tnxTower GPD Group 520 South Main St. Suite 2531 Akron, OH 44311 Phone: (330) 572-2100 FAX: (330) 572-2101	Job	6990 FL01	Page	5 of 7
	Project	2013723.04.6990.02	Date	07:25:09 11/25/13
	Client	MasTec Network Solutions	Designed by	mhoudeshell

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt lb	Allowable Load lb	Ratio Load Allowable	Allowable Ratio	Criteria
T7	81.2082	Diagonal	A325N	0.6250	3	5808.65	12425.20	0.467 ✓	1	Bolt Shear
		Horizontal	A325N	0.7500	3	3807.42	17892.40	0.213 ✓	1	Bolt Shear
		Leg	A325N	1.0000	6	30039.80	53014.40	0.567 ✓	1	Bolt Tension
		Diagonal	A325N	0.6250	3	5973.76	12425.20	0.481 ✓	1	Bolt Shear
T8	60.9999	Horizontal	A325N	0.7500	3	4161.67	17892.40	0.233 ✓	1	Bolt Shear
		Leg	A325N	1.0000	8	27530.10	53014.40	0.519 ✓	1	Bolt Tension
		Diagonal	A325N	0.6250	3	6259.07	12425.20	0.504 ✓	1	Bolt Shear
		Horizontal	A325N	0.7500	3	4593.57	17892.40	0.257 ✓	1	Bolt Shear
T9	40.6666	Leg	A325N	1.0000	8	32386.80	53014.40	0.611 ✓	1	Bolt Tension
		Diagonal	A325N	0.6250	3	6506.12	12425.20	0.524 ✓	1	Bolt Shear
		Horizontal	A325N	0.7500	3	5003.97	17892.40	0.280 ✓	1	Bolt Shear
		Diagonal	A325N	0.6250	6	4769.29	12425.20	0.384 ✓	1	Bolt Shear
T10	20.3333	Horizontal	A325N	0.7500	3	5379.05	17892.40	0.301 ✓	1	Bolt Shear

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	ϕP_{allow} lb	% Capacity	Pass Fail
T1	192.333 - 182.167	Leg	ROHN 2.5 STD	2	-2122.04	56631.20	3.7	Pass
T2	182.167 - 162	Leg	ROHN 2.5 STD	29	-15671.40	45132.70	34.7	Pass
T3	162 - 141.833	Leg	ROHN 3 STD	68	-50409.40	70434.00	71.6	Pass
T4	141.833 - 121.625	Leg	ROHN 4 STD	107	-84403.40	115687.00	73.0	Pass
T5	121.625 - 101.417	Leg	ROHN 5 EH	146	-112522.00	199811.00	56.3	Pass
T6	101.417 - 81.2082	Leg	ROHN 6 STD	173	-152502.00	202708.00	75.2	Pass
T7	81.2082 - 60.9999	Leg	ROHN 6 EH	200	-197874.00	302220.00	65.5	Pass
T8	60.9999 - 40.6666	Leg	ROHN 6 EH	227	-241949.00	301385.00	80.3	Pass
T9	40.6666 - 20.3333	Leg	ROHN 8 STD	254	-284892.00	332967.00	85.6	Pass
T10	20.3333 - 0	Leg	ROHN 8 STD	281	-305924.00	332963.00	91.9	Pass
T1	192.333 - 182.167	Diagonal	ROHN 1.5 STD	9	-2338.91	13001.30	18.0	Pass
T2	182.167 - 162	Diagonal	ROHN 1.5 STD	33	-7357.40	8755.79	84.0	Pass
T3	162 - 141.833	Diagonal	ROHN 2 STD	71	-8546.09	15700.50	54.4	Pass
T4	141.833 - 121.625	Diagonal	ROHN 2 EH	110	-8905.51	16964.30	52.5	Pass
T5	121.625 - 101.417	Diagonal	ROHN 2.5 STD	149	-11520.30	15972.30	72.1	Pass
T6	101.417 - 81.2082	Diagonal	ROHN 2.5 EH	176	-17426.00	17775.30	98.0	Pass
T7	81.2082 - 60.9999	Diagonal	ROHN 3 EH	203	-17921.30	31452.30	57.0	Pass
T8	60.9999 - 40.6666	Diagonal	ROHN 3 EH	230	-18777.20	27400.10	68.5	Pass
T9	40.6666 -	Diagonal	ROHN 3 STD	257	-19518.40	18913.20	103.2	Pass

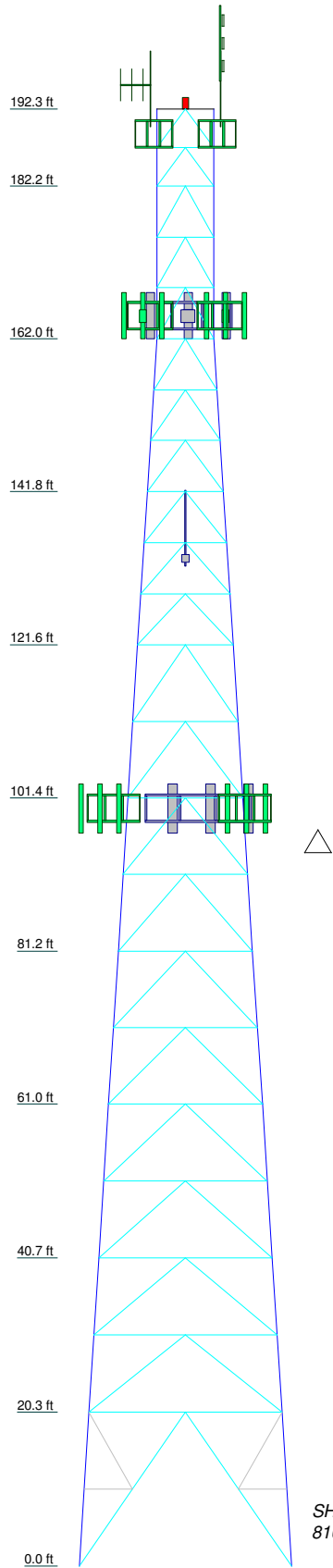
<i>tnxTower</i> GPD Group 520 South Main St. Suite 2531 Akron, OH 44311 Phone: (330) 572-2100 FAX: (330) 572-2101	Job	6990 FL01	Page	7 of 7
	Project	2013723.04.6990.02	Date	07:25:09 11/25/13
	Client	MasTec Network Solutions	Designed by	mhoudeshell

<i>Section No.</i>	<i>Elevation ft</i>	<i>Component Type</i>	<i>Size</i>	<i>Critical Element</i>	<i>P lb</i>	<i>ϕP_{allow} lb</i>	<i>% Capacity</i>	<i>Pass Fail</i>
						(T10) Redund Diag 1 Bracing	55.8	Pass
						(T10) Redund Hip 1 Bracing	0.4	Pass
						(T10) Redund Hip Diagonal Bracing	1.4	Pass
						(T10) Inner Bracing (T6)	0.6	Pass
						Bolt Checks	61.1	Pass
						Rating =	103.2	Pass

APPENDIX C

Tower Elevation Drawing

Section		T10	T9	T8	T7	T6	T5	T4	T3	T2	T1
Legs		ROHN 8 STD			ROHN 6 EH		ROHN 5 EH	ROHN 4 STD	ROHN 3 STD	ROHN 2.5 STD	
Leg Grade						A572-50					
Diagonals		Rohn 2.875"x.552"	ROHN 3 STD		ROHN 3 EH		ROHN 2.5 EH	ROHN 2 EH	ROHN 2 STD	ROHN 1.5 STD	
Diagonal Grade		44 ksi					A572-50				
Top Girts						N.A.				A	
Horizontals			ROHN 2.5 STD			ROHN 2 STD		ROHN 2 EH		ROHN 1.5 STD	
Red. Horizontals		ROHN 1.5 STD					N.A.				
Red. Diagonals		ROHN 2 STD					N.A.				
Red. Hips		ROHN 2 STD					N.A.				
Inner Bracing		ROHN 2.5 EH									
Face Width (ft)	28	25.42	L3 1/2x3 1/2x1/4	22.86	20.3	L3x3x1/4	17.74	15.18	12.82	10.06	7.5
# Panels @ (ft)		1 @ 20.3333	4 @ 10.1667	4 @ 10.1667	4 @ 10.1667	6 @ 10.1042	6 @ 10.1042	3 @ 6.7361	6 @ 6.72223	2 @ 5.08335	
Weight (lb)	30214.5	5366.5	4651.5	4694.3	4873.0	2634.4	2726.3	2143.2	1326.4	1015.3	599.7



DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
Flash Beacon Lighting	192.3	FR1A	165
8' Frame	189	RCMDC-4010-PF-48	165
8' Frame	189	2' Standoff	133
16 Element 20' x 2" Dipole	189	2" x 8' Omni	133
3 Element 18" x 12" Yagi	189	1' Square Dish	133
3" x 8' Omni	189	15' T-Boom	100
2" x 8' Omni	189	15' T-Boom	100
11.5' T-Frame	165	15' T-Boom	100
11.5' T-Frame	165	(3) 800-10865 w/ Mount Pipe	100
11.5' T-Frame	165	(3) 800-10865 w/ Mount Pipe	100
(3) APX17DWV-17DWV-S-E-ACU w/ Mount Pipe	165	(3) 800-10865 w/ Mount Pipe	100
(3) APX17DWV-17DWV-S-E-ACU w/ Mount Pipe	165	(3) RRUS-32	100
(3) APX17DWV-17DWV-S-E-ACU w/ Mount Pipe	165	(3) RRUS-32	100
(3) APX17DWV-17DWV-S-E-ACU w/ Mount Pipe	165	(3) RRUS-32	100
FRIG	165	RRUS 11	100
FRIG	165	RRUS 11	100
FRIG	165	RRUS 11	100
FXFB	165	DC6-48-60-18-8F Surge Suppression Unit	100
FXFB	165	DC6-48-60-18-8F Surge Suppression Unit	100
FXFB	165	DC6-48-60-18-8F Surge Suppression Unit	100
FR1A	165		
FR1A	165		

SYMBOL LIST

MARK	SIZE	MARK	SIZE
A	ROHN 1.5 STD		

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-50	50 ksi	65 ksi	44 ksi	44 ksi	60 ksi

TOWER DESIGN NOTES

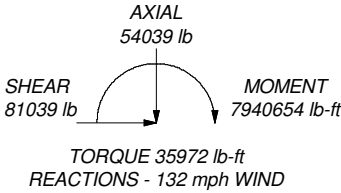
1. Tower is located in Broward County, Florida.
2. Tower designed for Exposure C to the TIA-222-G Standard.
3. Tower designed for a 132 mph basic wind in accordance with the TIA-222-G Standard.
4. Deflections are based upon a 60 mph wind.
5. Tower Structure Class II.
6. Topographic Category 1 with Crest Height of 0.00 ft
7. TOWER RATING: 103.2%


ALL REACTIONS
ARE FACTORED

MAX. CORNER REACTIONS AT BASE:

DOWN: 344819 lb
SHEAR: 47280 lb

UPLIFT: -313422 lb
SHEAR: 44863 lb





GPD Group
520 South Main St. Suite 2531
Akron, OH 44311
Phone: (330) 572-2100
FAX: (330) 572-2101

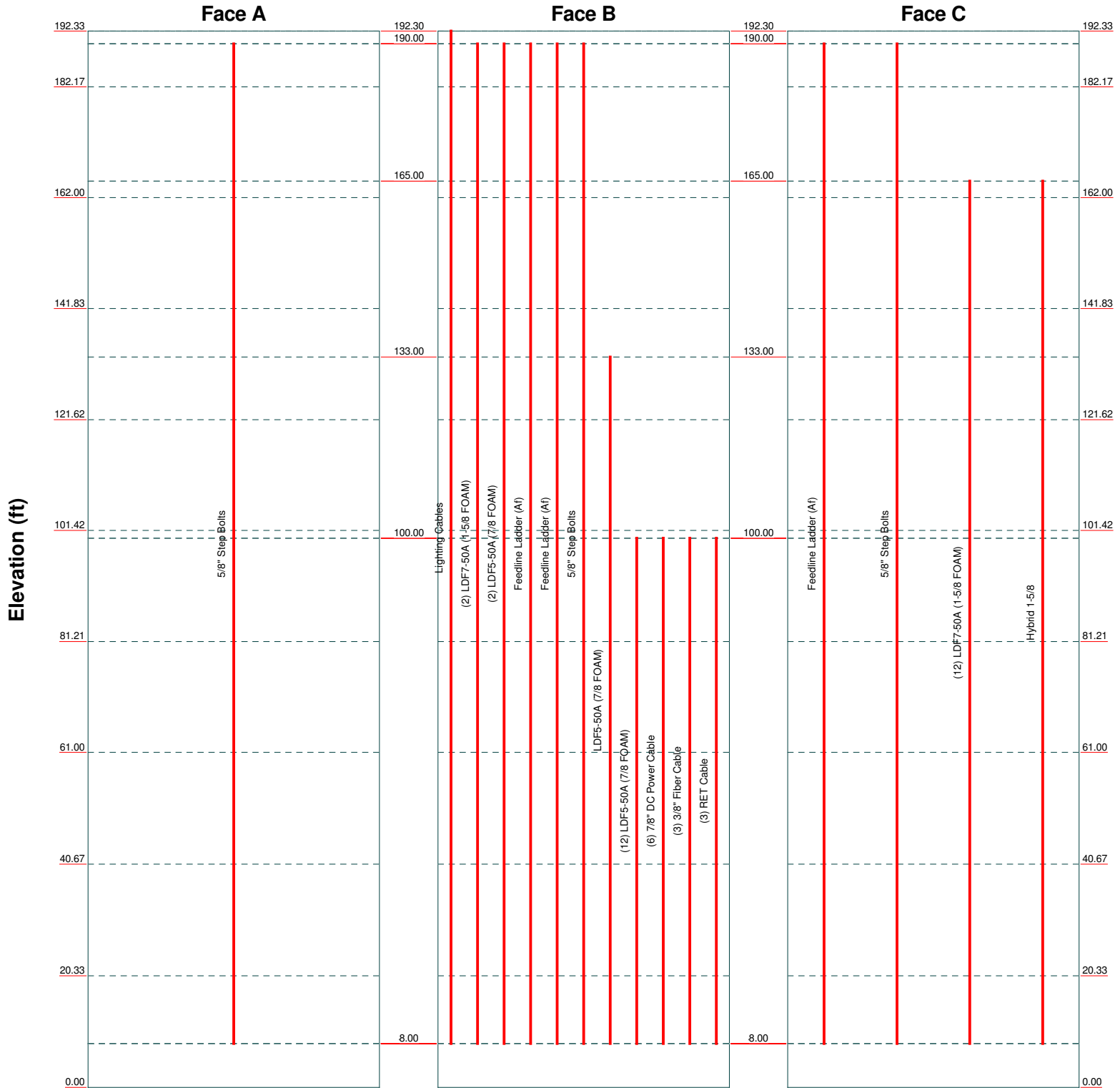
Job: **6990 FL01**
Project: **2013723.04.6990.02**

Client: MasTec Network Solutions	Drawn by: mhoudeshell	App'd:
Code: TIA-222-G	Date: 11/25/13	Scale: NTS
Path: N:\2011\ATandT\6990\7 2013723 04 6990 02 Nsoro SA\TNX\6990.eri		Dwg No. E-1

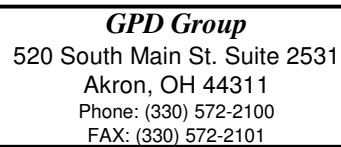
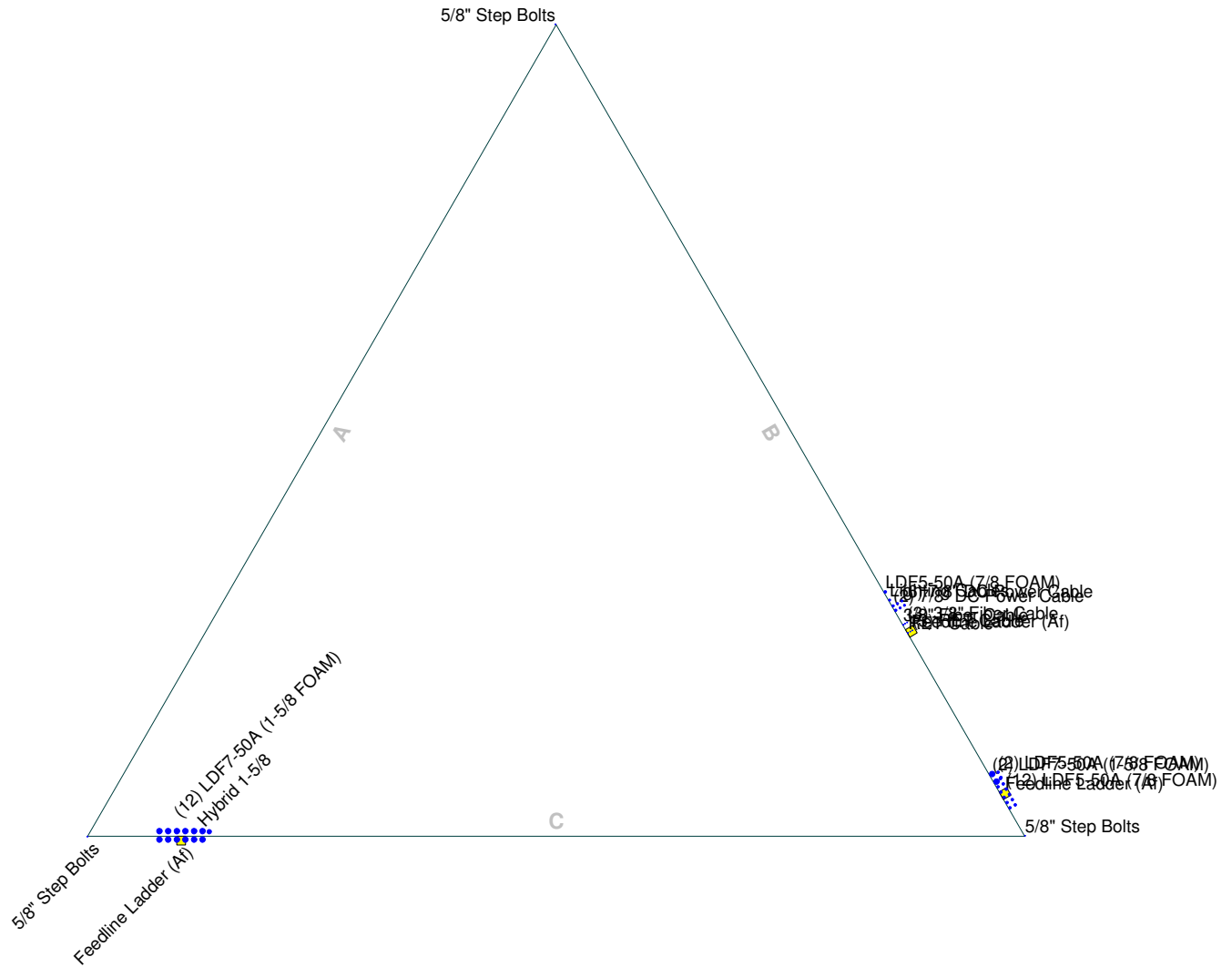
Feed Line Distribution Chart

0' - 192'3-31/32"

Round Flat App In Face App Out Face Truss Leg



Round Flat App In Face App Out Face



Path:	N:\2011\ATandT\6990\7 2013723 04 6990 02 Nsoro SA\TNX\6990.eri
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Dwg No. E-7

APPENDIX D

Anchor Rod Analysis



Self Support Anchor Rod Analysis (Rev G)
6990 FL01
2013723.04.6990.02

Anchor Rod Check per Section 4.9.9 of TIA-222-G

Number of Anchor Rods=	8
Anchor Rod Grade=	A354-BC
Diameter of Anchor Rod=	1 in
V_u =	47.28 k
P_u =	344.819 k
F_{ub} =	125 ksi
A_n =	0.6060 in ²
R_{nt} =	75.75 k
ϕ =	0.8
n =	0.5 TIA-222-G Figure 4-4 & section 4.9.9
Interaction=	0.9063
Percent Capacity=	90.6% OK

APPENDIX E

Foundation Analysis



Self Support Tower Caisson Analysis - Rev G
6990 FL01
2013723.04.6990.02 (skin friction adjusted to account for collar)

Tower Reactions	
Uplift	313.4 kips
Compression	344.8 kips

Caisson Details	
Diameter	4 ft
Height Above Grade	0.25 ft
Depth Below Grade	50.75 ft
Dead Load Factor	1.2
Crosssectional Area	12.6 ft ²
Perimeter	12.6 ft

(TIA-222-G-1 Section 2.3.2)

Reinforcement Properties	
Reinforcing Known	No
Vertical Bar Size	#8
# of Existing Vertical Bars	12
Horizontal Bar Type	Tie
Horizontal Bar Size	#4
Anchor Rod Embedment	110 in
Anchor Rod Circle	12 in
Min. Concrete Cover	3 in
f_c'	3000 psi
F_y	60 ksi

Soil Properties	
Water Table Depth	2 ft
Bearing Type	Net
Ultimate End Bearing	4 ksf
ϕ (bearing)	0.75
ϕ (skin friction - uplift)	0.75
ϕ (skin friction - comp.)	0.75

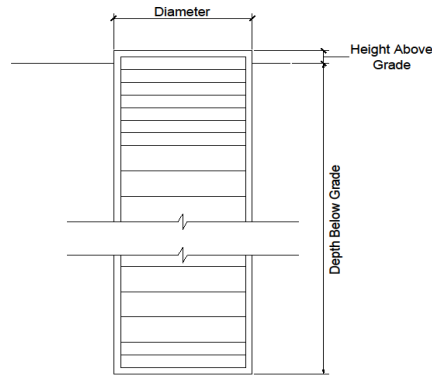
(TIA-222-G-1 Section 9.4.1)

(TIA-222-G-1 Section 9.4.1)

(TIA-222-G-1 Section 9.4.1)

Overall Capacities		
Compression Capacity	142.5%	NG
Uplift Capacity	134.5%	NG
Reinforcement Capacity	61.6%	OK
As Min OK?	Yes	OK
Controlling Capacity	142.5%	NG

← Reinforcing steel unknown - minimums assumed (see report), field verification is recommended.



Ultimate					
Soil Layer	Soil Layer Thickness (ft)	Uplift Skin Friction (ksf)	Compression Skin Friction (ksf)	Soil Unit Weight (pcf)	Concrete Dry Unit Weight (pcf)
1 (neglected)	3	0.000	0.000	0.105	0.150
2	2	0.198	0.282	0.105	0.150
3	2.75	0.520	0.748	0.115	0.150
4	2.25	0.136	0.000	0.115	0.150
5	2.75	0.218	0.000	0.115	0.150
6	7.25	0.218	0.312	0.115	0.150
7	10	0.322	0.458	0.110	0.150
8	10	0.428	0.610	0.115	0.150
9	10.75	0.536	0.766	0.115	0.150
Totals	50.75				

Soil Check							
Soil Layer	Soil Layer Thickness (ft)	Effective Soil Unit Weight (pcf)	Effective Concrete Unit Weight (pcf)	Uplift Skin Friction Resistance (kips)	Compression Skin Friction Resistance (kips)	Effective Soil Weight Removed (kips)	Effective Concrete Weight Added (kips)
1 (neglected)	3.0	0.043	0.088	0	0	1.61	3.58
2	2.0	0.043	0.088	5	7	1.07	2.20
3	2.8	0.053	0.088	18	26	1.82	3.03
4	2.3	0.053	0.088	4	0	1.49	2.48
5	2.8	0.053	0.088	8	0	1.82	3.03
6	7.3	0.053	0.088	20	28	4.79	7.98
7	10.0	0.048	0.088	40	58	5.98	11.01
8	10.0	0.053	0.088	54	77	6.61	11.01
9	10.8	0.053	0.088	72	103	7.11	11.83
Totals	50.75			220.8	299.0	32.3	56.1

End Bearing Resistance:	37.7 kips	Caisson Weight Resistance:	67.4 kips
Compression Skin Friction Resistance:	224.3 kips	Uplift Skin Friction Resistance:	165.6 kips
Total Compression Resistance:	262.0 kips	Total Uplift Resistance:	233.0 kips

Reinforcement Check	
Compression	
A_{sc}	9.4 in ²
A_s	1809.6 in ²
ϕ (compression)	0.7
ϕP_n	2887.3 k
Compression Capacity	14.3% OK
Reinforcement Minimum	
A_s (effective)	904.7786842 in ²
Compression A_s min. (in ²)	9.0 OK
Tension	
Rebar Cage Diameter	40.0 in
$R_{q/d}$ Development Length	54.8 in
Development Length (in)	93.0 OK
T_u	313.4 k
Tensile Strength, ϕP_u (kip)	508.9
Tensile Capacity	61.6% OK

(ACI 318-05 Section C.3.2.2)

(ACI 318-05 Section 10.3.6)

(ACI 318-05 Section 10.8.4)

(ACI 318-05 Section 10.9.1)

(ACI 318-05 Section 12.2.2)

**GPD GROUP**

Engineers • Architects • Planners

Job 2013723.04, 6990.02Calculated By MH Date 11-25-13

Sheet No. _____ Of _____

Checked By _____ Date _____

Caisson w/ Collar Check

TOX Reactions: Uplift = 313,422k
 Compression = 344,819k

$$\text{Collar Weight} = 0.15(2.25')[(12' \times 12') - (4')^2(\pi/4)] + 0.0876(5.75')[(12' \times 12') - (4')^2(\pi/4)]$$

$$= 44.36k + 66.20k = 110.56k$$

Uplift Check

resistance from Spreadsheet = 216.2k

$$\text{total resistance} = 216.2 + 0.9(110.56k) = 315.7k$$

$$\text{Capacity} = \frac{313.422k}{315.7k} \times 100 = \underline{\underline{99.3\%}}$$

Compression Check

resistance from Spreadsheet = 262.0k

$$\text{Collar Bearing} = [(12' \times 12') - 4^2(\pi/4)](4kcf)(0.75) = 394.3k$$

$$\text{total resistance} = 262k + 394.3k = 656.3k$$

$$\text{Capacity} = \frac{344.819k + 1.2(110.56k)}{656.3k} \times 100 = \underline{\underline{72.8\%}}$$